Low-voltage pseudo-differential transconductor with improved tunability-linearity trade-off

B. Calvo, S. Celma, J. Ramírez-Angulo and M.T. Sanz

A new low-voltage pseudo-differential CMOS transconductor using transistors in the saturation region is presented. It keeps the input common-mode voltage constant, while its transconductance is easily tunable through a DC voltage preserving linearity for a moderate range of G_m values. Post-layout results for a 2.7 V–0.5 µm CMOS design dissipating less than 1.5 mW show a 1:2 G_m tuning range with an almost constant bandwidth over 600 MHz. Total harmonic distortion figures are below -60 dB over the whole range at 10 MHz up to a 100 µA_{p-p} differential output.

Introduction: The ground referred differential pair using transistors in the saturation region with balanced input signals meets the currently demanded low-voltage (LV) requirement. High transconductance G_m values can also be obtained, thus making it an appealing choice for high-frequency operation. However, the only way to tune the G_m – necessary for compensation of fabrication tolerances and to achieve programmability of filter parameters – is through the input common-mode bias voltage V_{CM} . This modifies the transistors' biasing point and directly affects the linearity since the third-harmonic distortion is inversely proportional to the pair transistors' gate overdrive voltage $V_{cd} = V_{CM} - V_{TH}$ [1]. In addition, this issue is critical for LV applications where the signal swing, inherently constrained to a small headroom voltage, would be further limited owing to V_{CM} variations.

Transconductance amplifier architecture and performances: To overcome the drawbacks derived from changing V_{CM} for tuning purposes, the pseudo-differential stage shown in Fig. 1 is proposed. Each transistor in the classical pseudo-differential pair is split into matched transistors $M_{1A}-M_{1B}$ and $M_{2A}-M_{2B}$ that form differential pairs. Fully balanced input signals $V_{CM}+(1/2)V_{\rm in}, V_{CM}-(1/2)V_{\rm in}$ are applied to M_{1A} and M_{2A} , which act as improved voltage followers thanks to the negative feedback G_m -boosting introduced through M_3 [2]. In consequence, input signals are accurately translated to the source of M_B transistors. Both M_{1B} and M_{2B} gates are driven by a bias voltage $V_{CM}+V_{gain}$. Then, given that M_{1A} and M_{1B} are equally sized and matched, the DC current through M_{1B} will replicate the current in M_{1A} , with a gain which will depend on the voltage V_{gain} . Transistor M_3 takes in M_{1B} current changes.

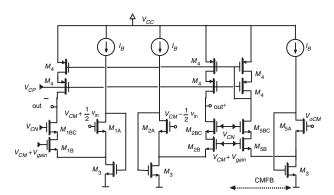


Fig. 1 Proposed pseudo-differential amplifier

Straightforward analysis of this stage shows that the output differential current is given by

$$I_O = I_{\mathrm{out}}^+ - I_{\mathrm{out}}^- = 2K(V_{\mathit{CM}} + V_{\mathit{gain}} - V_{\mathit{TH}})V_{\mathrm{in}}$$

where V_{TH} is the threshold voltage of $M_{\rm B}$ transistors and $K = (1/2)\mu C_{OX}(W/L)_{\rm B}$. This simple scheme thus makes it possible to hold the input common-mode voltage V_{CM} constant, keeping it separate from the transconductance adjustment V_{gain} signal while, as will be shown next, linearity is independent of V_{gain} for a moderate G_m tuning range. The cell in Fig. 1 has been designed in a standard 0.5 μ m CMOS

The cell in Fig. 1 has been designed in a standard $0.5~\mu m$ CMOS process with a 2.7~V single supply and a bias current of $50~\mu A$. Highswing cascode current mirrors have been used to maximise signal swing

while improving mirroring. Cascode transistors, $M_{1\mathrm{BC}}$ and $M_{2\mathrm{BC}}$, have been introduced to increase the output resistance up to the M Ω range. To set the adequate output common-mode voltage V_{oCM} , equal to V_{CM} , while properly delivering the required output adaptive current over the whole tuning range, a replica of the single-ended pseudo-differential stage has been employed. The gate of $M_{5\mathrm{B}}$ is biased with $V_{CM} + V_{gain}$, while that of $M_{5\mathrm{A}}$ is driven by V_{oCM} , whose detection is realised by using two 1 pF capacitors (not shown). The resulting topology is very compact and a maximum $\pm 0.1\%$ V_{CM} variation over the entire G_m tuning range is predicted by simulations. The V_{CM} has been set to 1.7 V so as to obtain a maximum voltage swing of $0.8~\mathrm{V_{p-p}}$ on each input while maintaining M_{A} , M_{3} in saturation.

Post-layout results using Spectre with a BSIM3v3.2 level 53 transistor model show a 1:2 G_m tuning for V_{gain} varying from -0.1 to +0.1 V, with a bandwidth almost constant above 600 MHz (Fig. 2). For the nominal value $V_{gain} = 0 \text{ V}$ the current through output transistors is $I_{\text{out}} = 50 \,\mu\text{A}$ and the power dissipation is 1.08 mW. For $V_{gain} = -0.1 \,\text{V}$ and +0.1 V, the currents though output transistors are approximately 25 and 100 µA, and the power consumption 0.88 and 1.46 mW, respectively. To keep moderate consumption, the maximum value for I_{out} that will be considered is 100 μA. The total harmonic distortion figures at 10 MHz (Fig. 3) are below -60 dB over the whole tuning range up to a $100 \, \mu A_{p-p}$ differential output. If we compare these THD levels to those achieved by the conventional pseudo-differential pair with equal transistor sizes, bias current and transconductance values, both structures provide comparable results for $V_{gain} = 0 \text{ V}$ and +0.1 V. However, when reducing V_{od} i.e. for $V_{gain} = -0.1$ V, the proposed circuit preserves the THD in contrast with the distortion degradation that the classical pseudo-differential pair exhibits, as shown in Fig. 3. The obtained THD improvement for a 100 $\mu A_{\text{p-p}}$ differential output is as high as 10 dB. The CMRR at low frequencies is 77, 73 and 64 dB for V_{gain} = -0.1, 0 and +0.1 V, respectively. These CMRR figures are similar to those reported for other CMOS pseudo-differential pairs using transistors in the saturation region [3, 4], all tuned through V_{CM} with the inherent constraints it poses. The input referred noise spectral density is 15 nV/ $\sqrt{\text{Hz}}$ at 50 MHz.

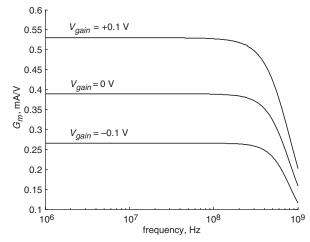


Fig. 2 Frequency response for $V_{gain} = -0.1$, 0, +0.1 V

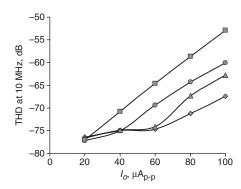


Fig. 3 *THD at 10 MHz* G_m corresponding to +0.1 V ($-\spadesuit-$), 0 V ($-\spadesuit-$) and -0.1 V: ($-\spadesuit-$) proposed and ($-\blacksquare-$) classical pseudo-differential pair

Conclusions: A new low-voltage CMOS pseudo-differential pair has been presented, which offers moderate continuous tunability over the video frequency range preserving a good linearity while keeping constant the input common-mode voltage. The proposed cell is thus an appealing choice in present-day mixed signal applications.

Acknowledgments: This work has been supported by DGA (PIP/187-2005) and MCYT-FEDER (TIC2005-00285/MIC).

© The Institution of Engineering and Technology 2006 6 June 2006

Electronics Letters online no: 20061772

doi: 10.1049/el:20061772

B. Calvo, S. Celma and M.T. Sanz (Group of Electronic Design, University of Zaragoza, E-50009 Zaragoza, Spain)

E-mail: becalvo@unizar.es

J. Ramírez-Angulo (Klipsh School of Electrical and Computer Engineering, New Mexico State University, Las Cruces, NM 88003, USA)

References

- 1 Sánchez-Sinencio, E., and Silva-Martínez, J.: 'CMOS transconductance amplifiers and active filters: a tutorial', *IEE Proc., Circuits Devices Syst.*, 2000, 147, (1), pp. 3–12
- 2 Ramírez-Angulo, J., Carvajal, R.G., Torralba, A., Galán, J.A., Vega-Leal, A.P., and Thombs, J.: 'The flipped voltage follower: a useful cell for low-voltage low-power circuit design'. Proc. IEEE Int. Symp. on Circuits and Systems, 2002, Vol. 3, pp. 615–618
- 3 Baschirotto, A., Rezzi, F., and Castello, R.: 'Low-voltage balanced transconductor with high input common-mode rejection', *Electron. Lett.*, 1994, 30, (20), pp. 1669–1670
- 4 Mohieldin, A.N., Sánchez-Sinencio, E., and Silva-Martínez, J.: 'A fully balanced pseudo-differential OTA with common mode feedforward and common mode feedback detector', *IEEE Int. J. Solid-State Circuits*, 2003, 38, (4), pp. 663–667